



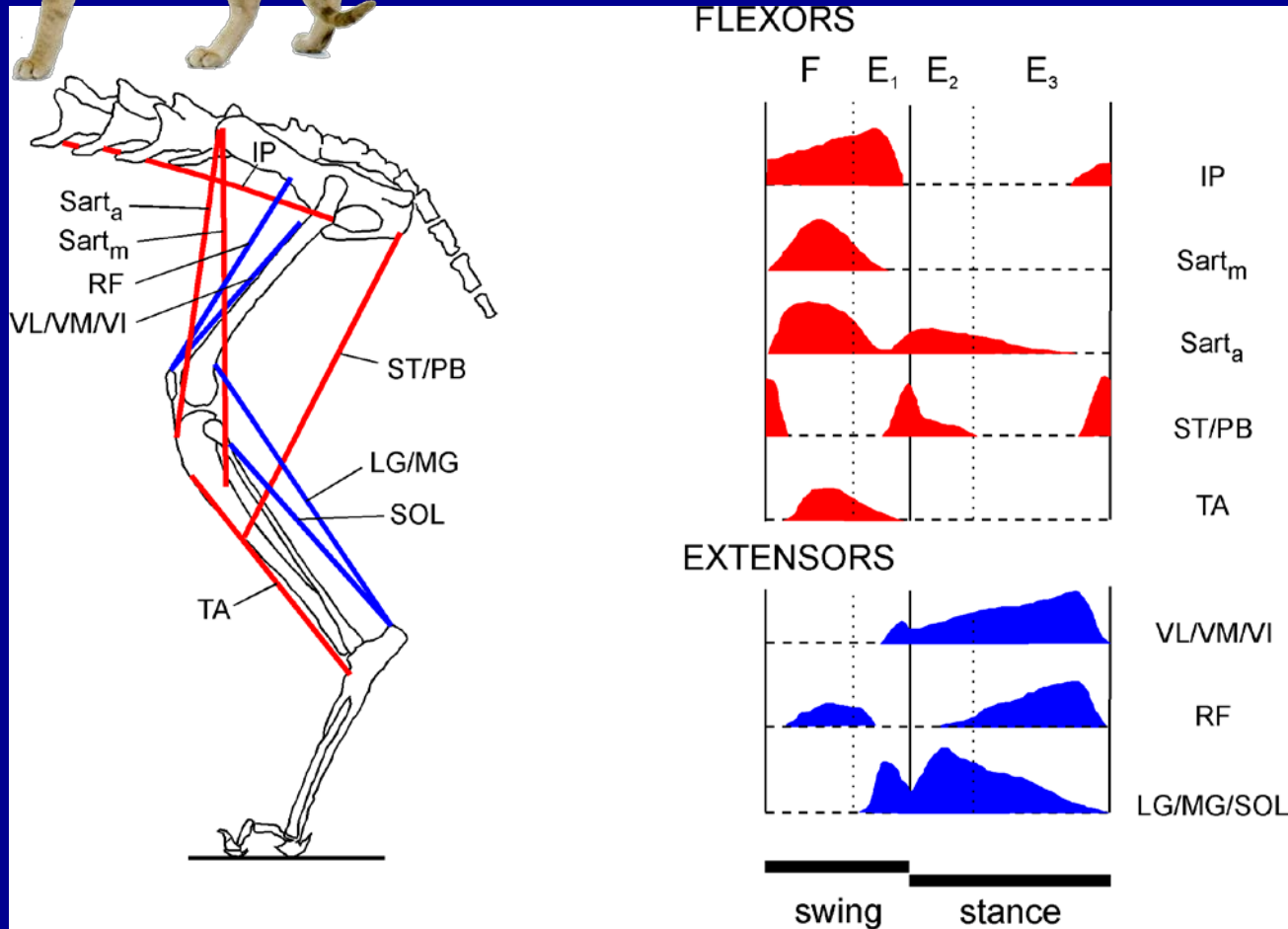
Tensegrity Engineering for Space Systems

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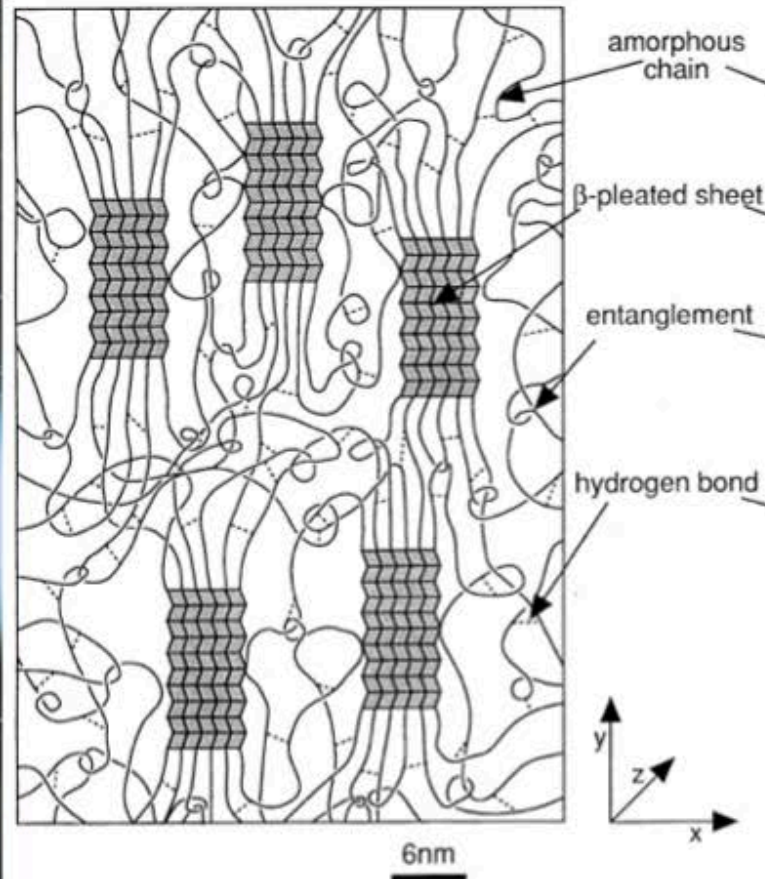
Professor Emeritus, UCSD

TIAS Faculty Fellow Texas A&M

First Motivation: Animal Locomotion

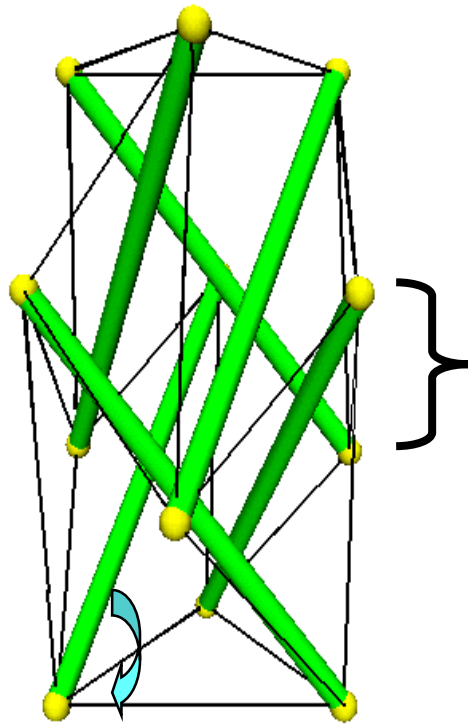


The dragline silk of a *Nephila Clavipes*

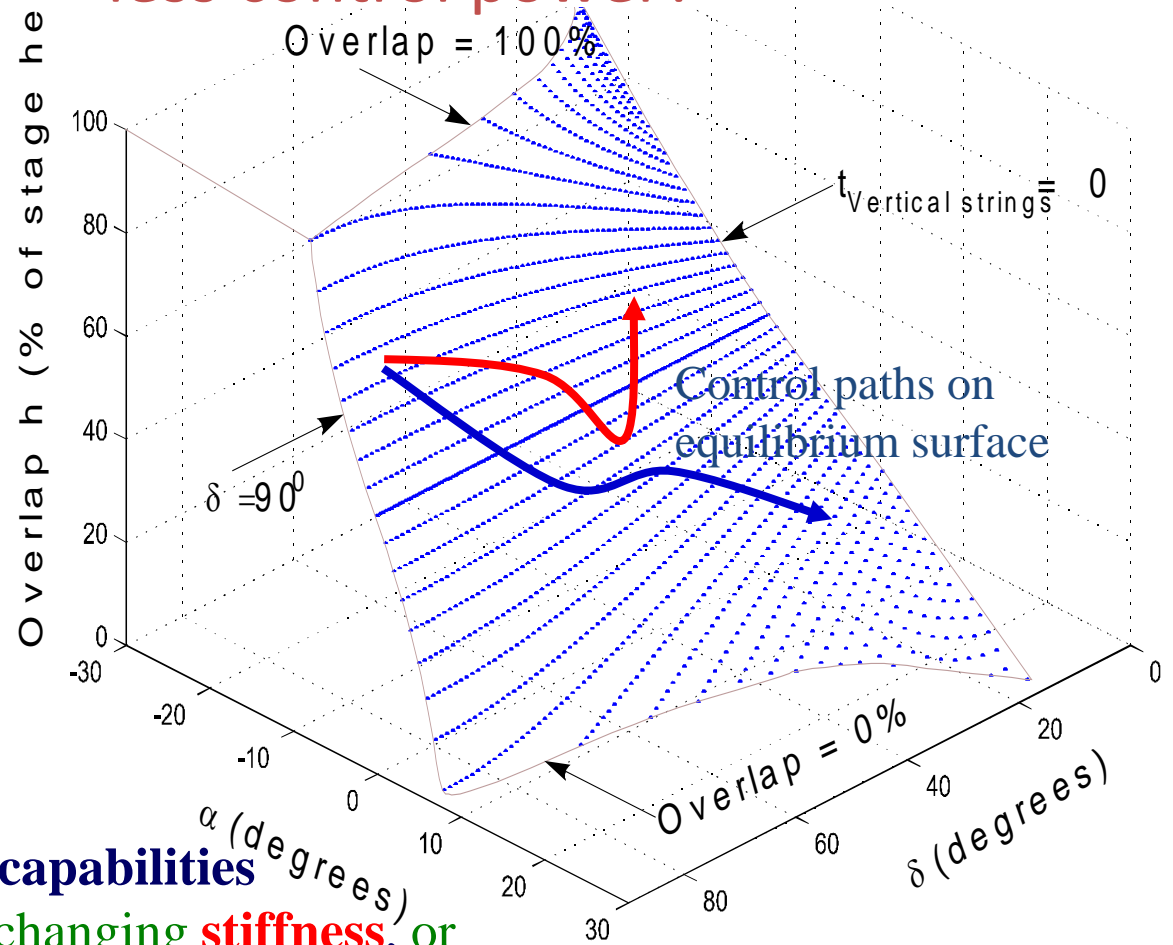


The molecular structure of nature's strongest fiber.

The rigid bodies are the β -pleated sheets, and the tensile members are the amorphous strands that connect to the β -pleated sheets



Why Tensegrity uses less control power?



Two unique tensegrity capabilities

- Change **shape** without changing **stiffness**, or
- Change **stiffness** without changing **shape**

Class 1 Tensegrity Dynamics

Let rigid rods and massless elastic strings be connected as

$$\begin{bmatrix} B & R & S \end{bmatrix} = N \begin{bmatrix} C_b^T & C_r^T & C_s^T \end{bmatrix}, \quad \text{Then}$$

$$\ddot{N}M + NK(\gamma, \dot{N}, W) = W$$

$$M = C_b^T \hat{m} C_b \frac{1}{12} + C_r^T \hat{m} C_r, \quad K(\gamma, \dot{N}, W) = C_s^T \hat{\gamma} C_s - C_b^T \hat{\lambda} C_b$$

where

$$-\hat{\lambda} = \left[\dot{B}^T \dot{B} \right] \hat{m} \hat{l}^{-2} \frac{1}{12} + \left[B^T F(\gamma) C_b^T \right] \hat{l}^{-2} \frac{1}{2}, \quad F(\gamma) = W - S \hat{\gamma} C_s$$

$$\lambda_i = \frac{\text{force in bar } b_i}{\|b_i\|},$$

$$\gamma_i = \frac{\text{force in string } s_i}{\|s_i\|}$$

Active Form-Finding

Feedback Control to converge to a specified desired shape \bar{Y} :

$$\ddot{N}M + NK(\gamma) = W, \quad K(\gamma) = C^T \Sigma C, \quad Y(t) = LN(t)R = \text{current shape}$$

$$\Sigma = \begin{bmatrix} -\hat{\lambda} & 0 \\ 0 & \hat{\gamma} \end{bmatrix}, \quad \begin{bmatrix} B & S \end{bmatrix} = NC^T, \quad C^T = \begin{bmatrix} C_b^T & C_s^T \end{bmatrix},$$

$$\hat{\lambda} = \frac{1}{12} \hat{l}^{-2} \left[6B^T (W - S\hat{\gamma}C_s) C_b^T - \dot{B}^T \dot{B}^T \hat{m} \right] = \text{a diagonal matrix}$$

Control objective: $Y(t) \rightarrow \bar{Y}$.

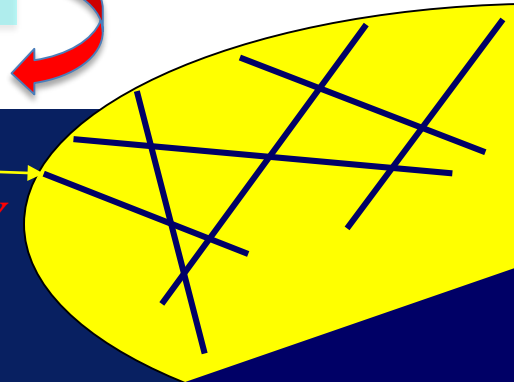
Find the control γ to cause the error $\Omega(t) = Y(t) - \bar{Y}$

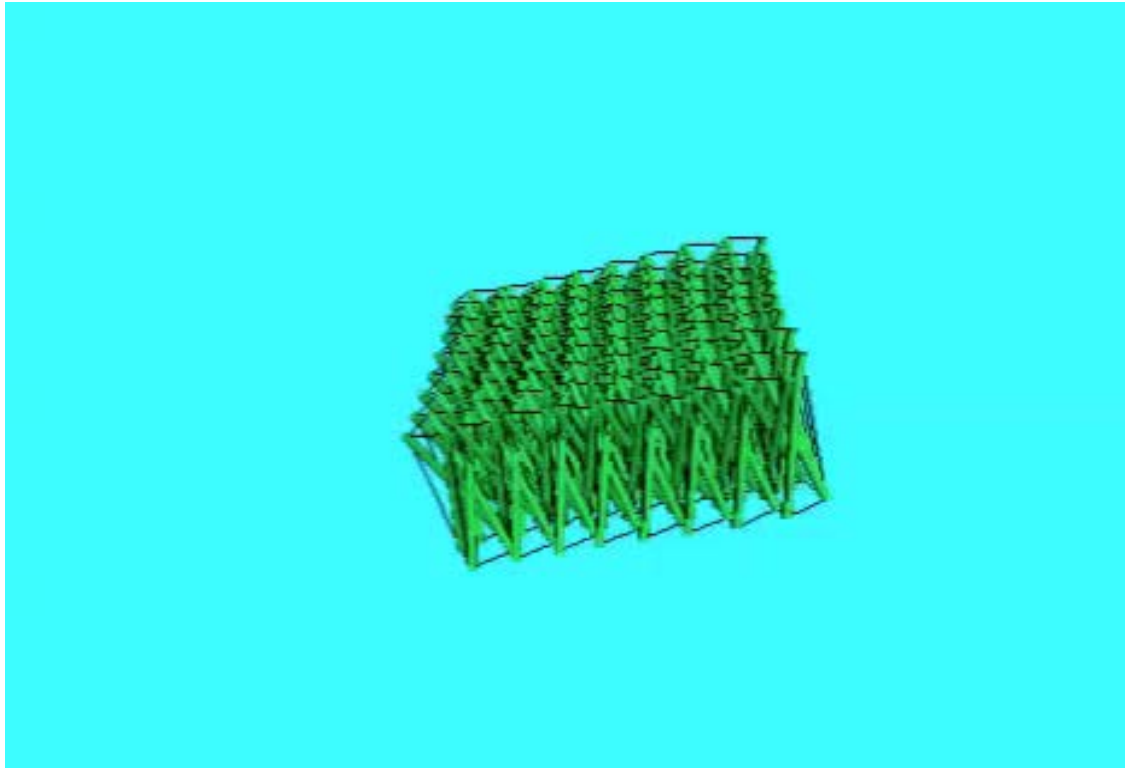
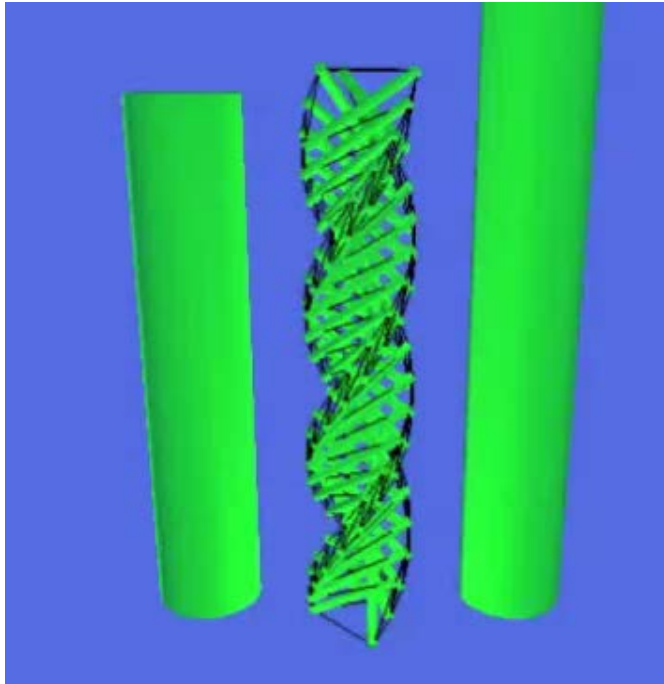
to satisfy a stable eq

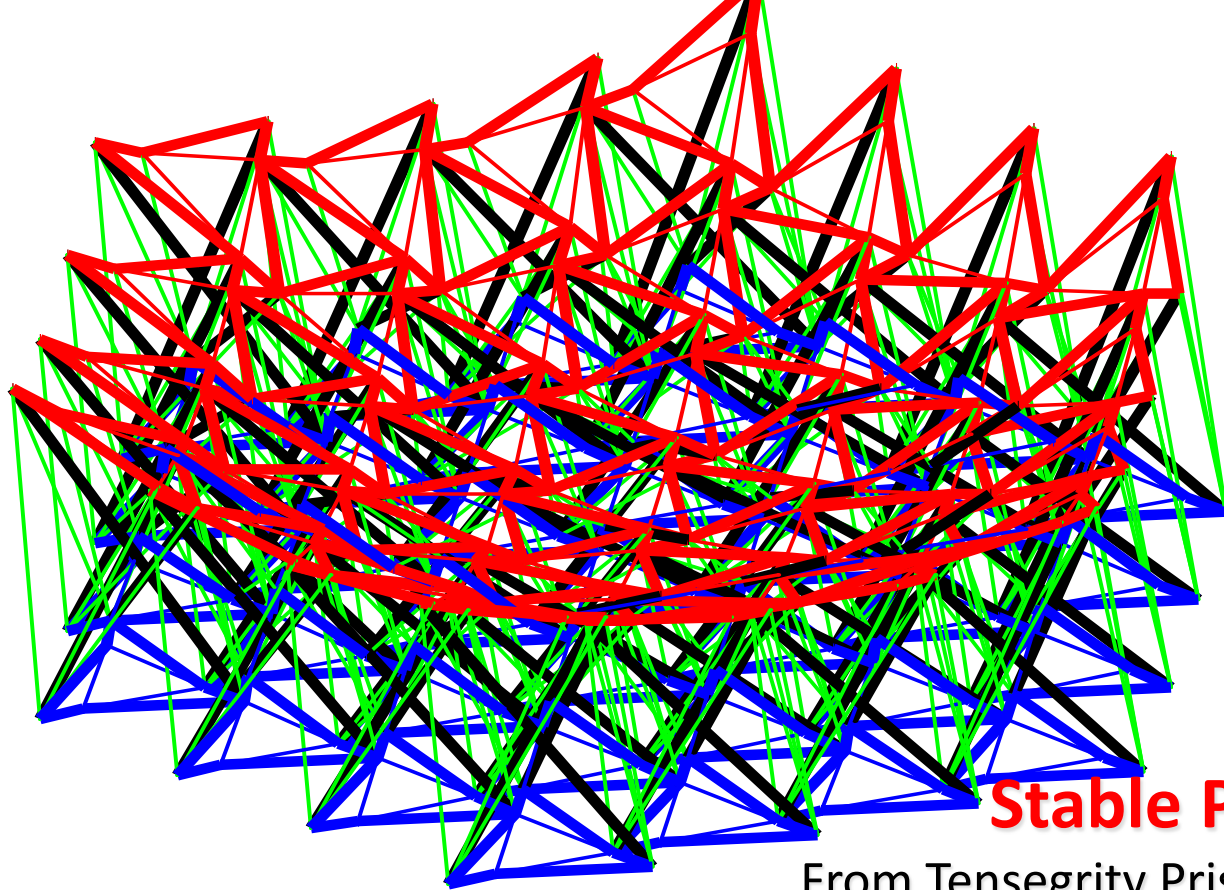
$$\ddot{\Omega} + P\dot{\Omega} + Q\Omega = 0$$

LINEAR in $\gamma(N(t), \dot{N}(t), W(t))$!!

Desired shape
(Location of selected nodes) Y



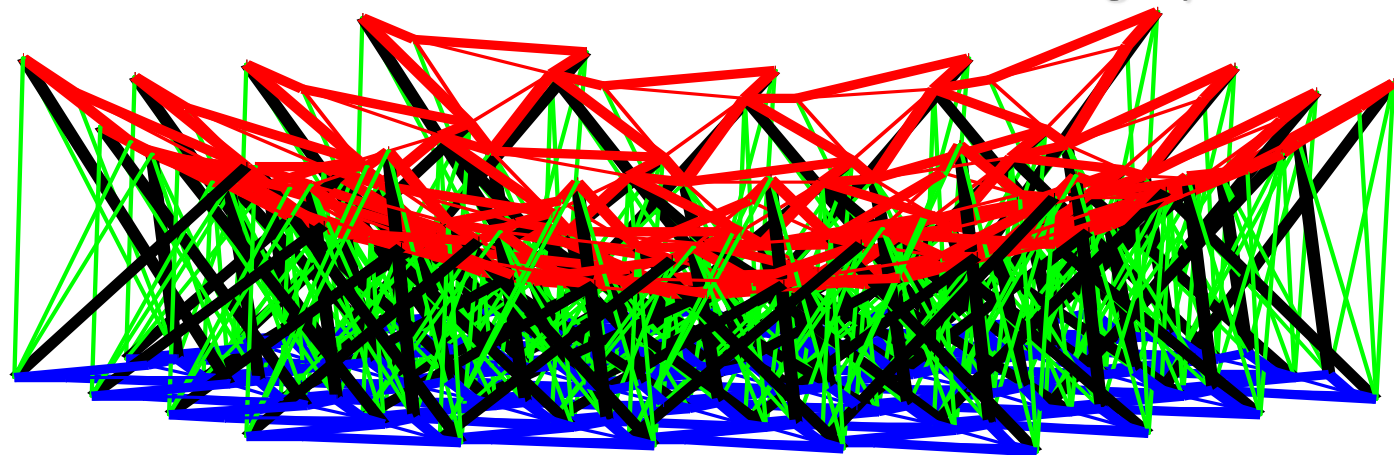




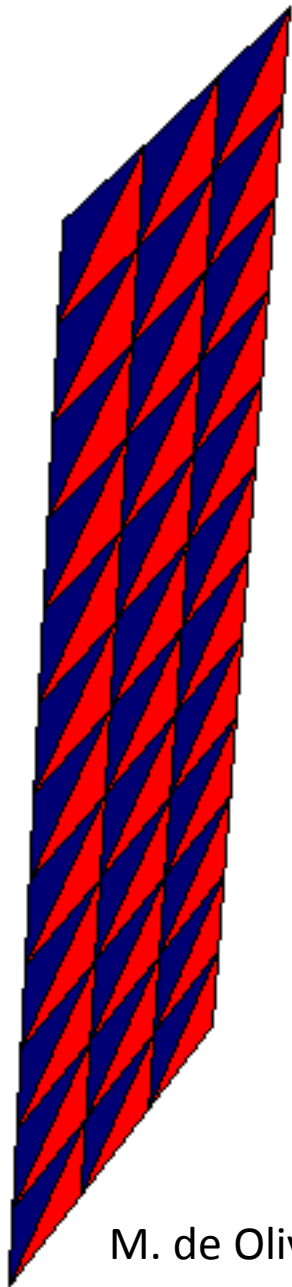
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Stable Parabolic Surface

From Tensegrity Prisms with no soft modes



Integrate Design of Origami/Tensegrity



M. de Oliveira

Tensegrity: 3D structures from 1D objects
(High strength, high stability, low mass, deployable)

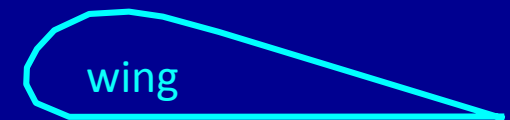
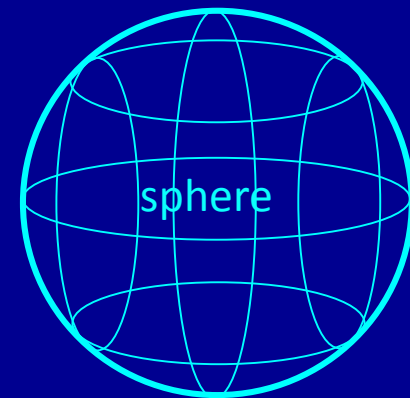
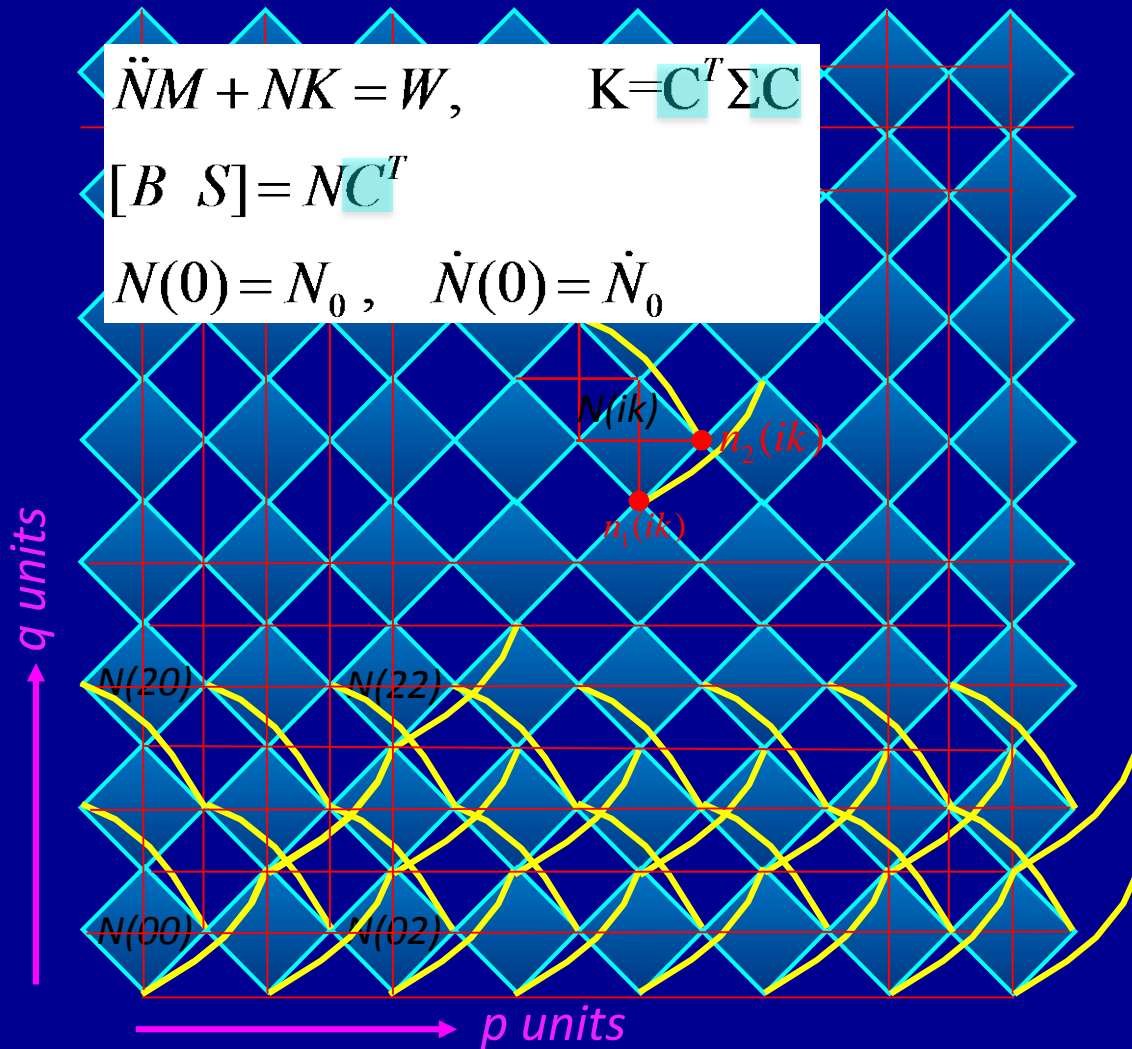
Origami: 3D structures from 2D objects
(low strength, low stability, foldable)

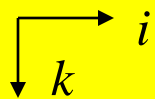
Double Helix Tensegrity (DHT)

$$\ddot{N}M + NK = W, \quad K = C^T \Sigma C$$

$$[B \ S] = NC^T$$

$$N(0) = N_0, \quad \dot{N}(0) = \dot{N}_0$$





$$R = 1, r = 0.2$$

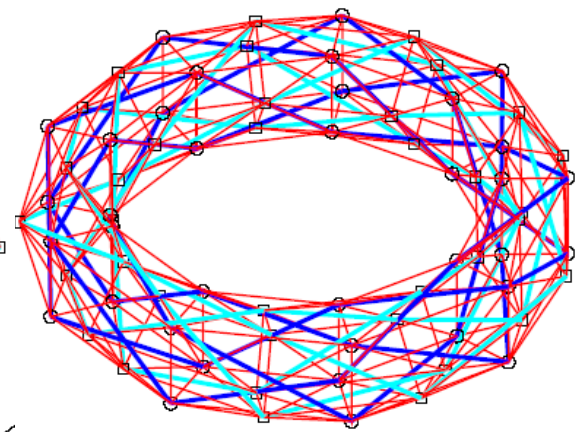
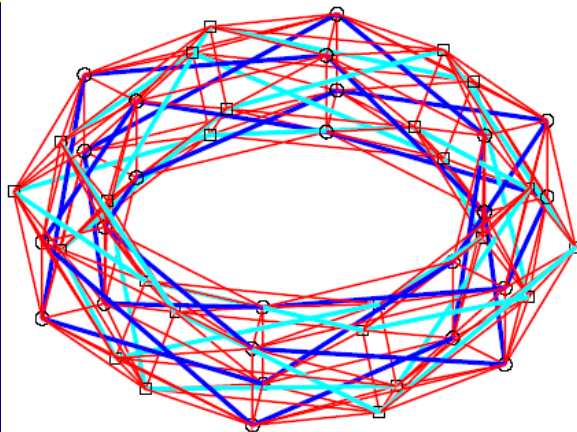
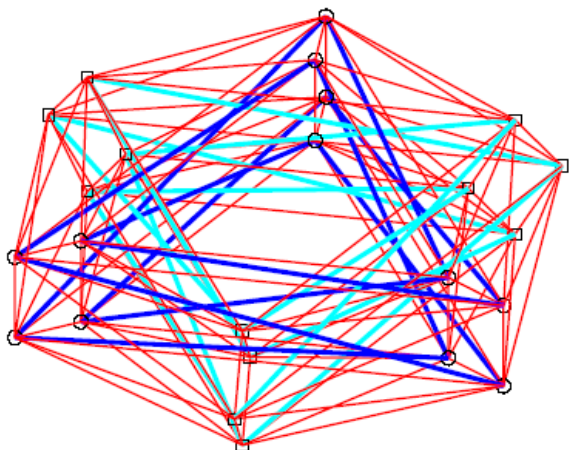
Torus

$q = 3$

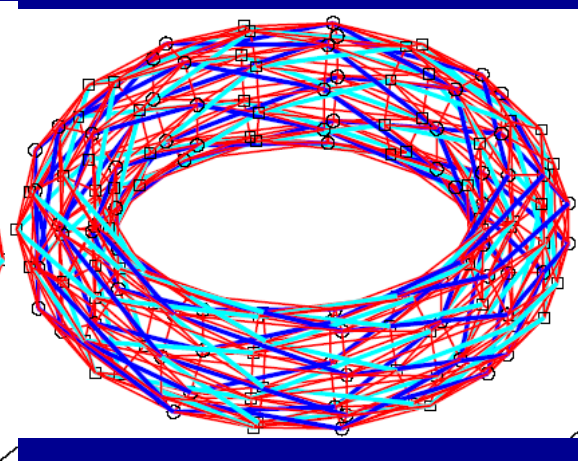
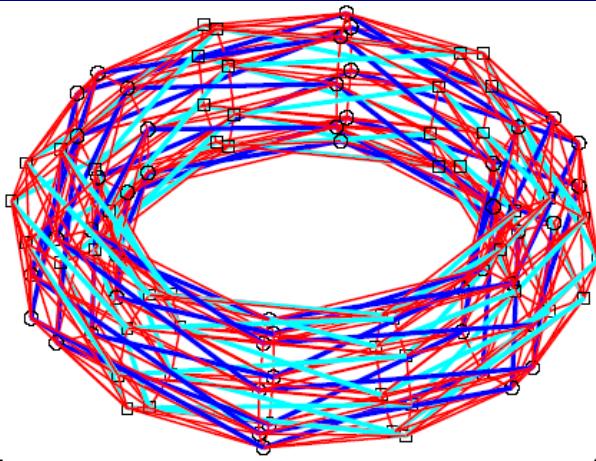
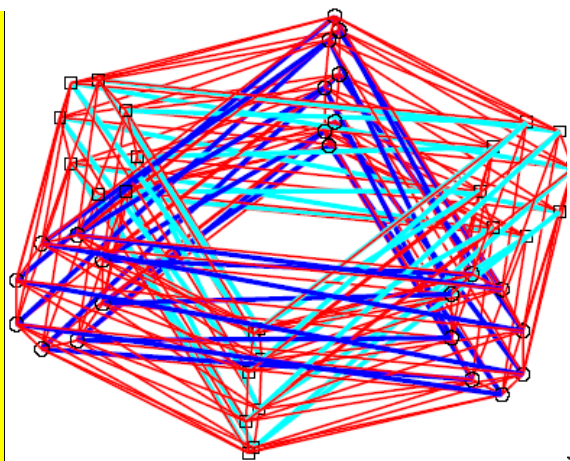
$q = 6$

$q = 9$

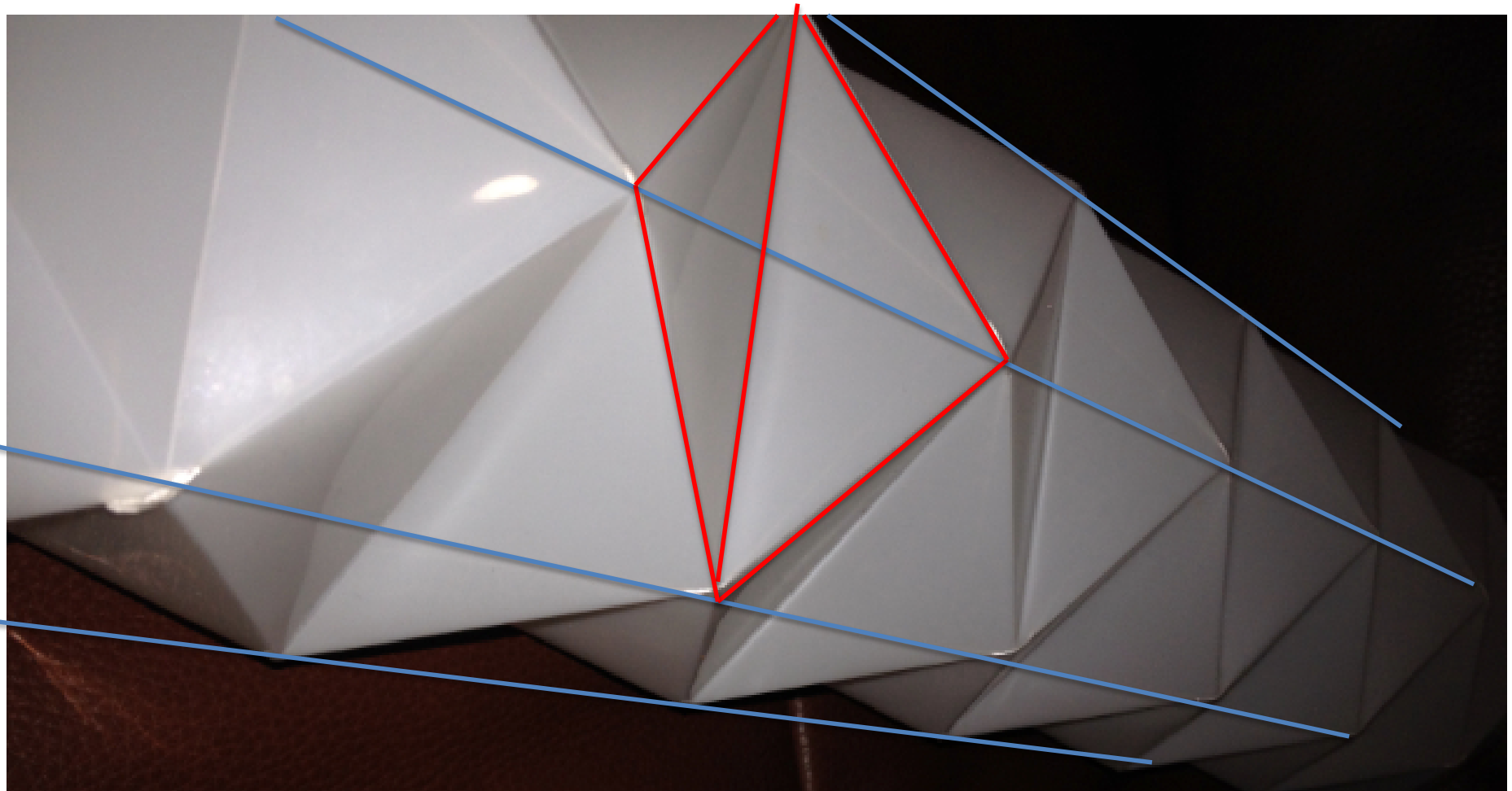
$p = 4$



$p = 8$



Double Helix Tensegrity (DHT): Exterior View

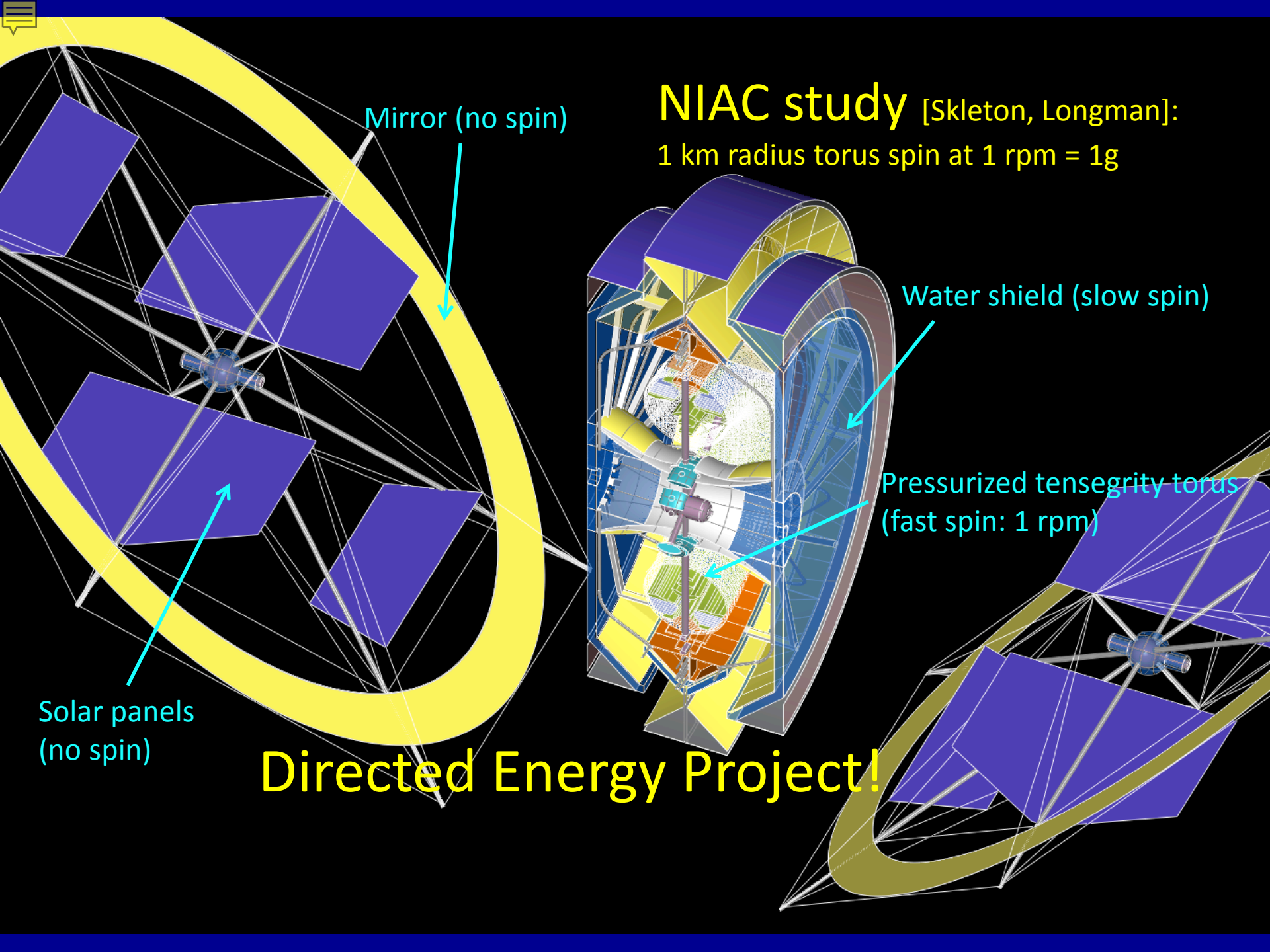




Primal and Dual DHT

Primal DHT: White lines are compressive members
Edges are **tensile** members

Dual DHT: White lines are **tensile** members (cables)
Edges are compressive members



NIAC study [Skleton, Longman]:

1 km radius torus spin at 1 rpm = 1g

Mirror (no spin)

Water shield (slow spin)

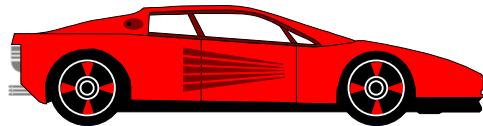
Pressurized tensegrity torus (fast spin: 1 rpm)

Solar panels (no spin)

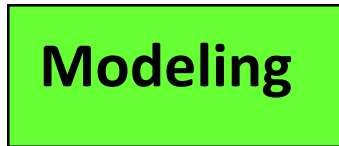
Directed Energy Project!

We Need Tools to Pin the Tail on the Performance Limiting Technology

From first principles, Universities teach component technology

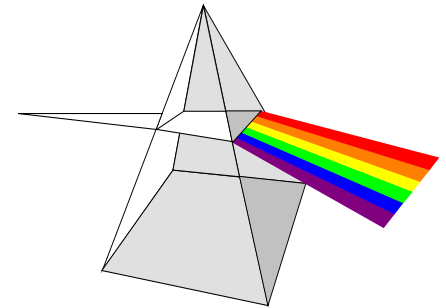
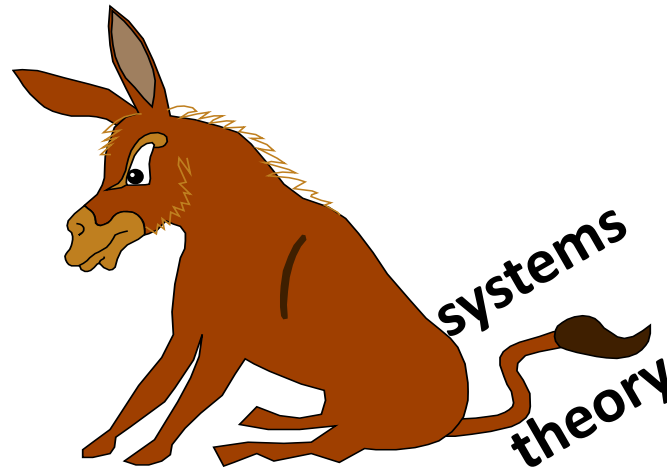
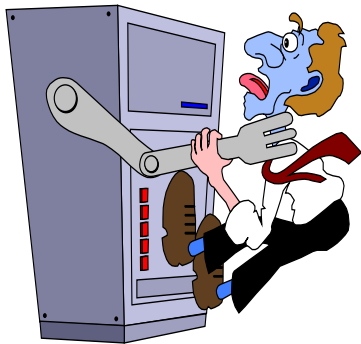


Design/Mfg

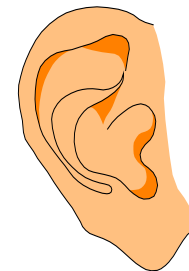
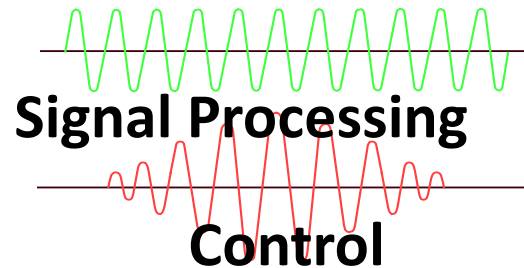


Modeling

Computing



Physics



Sensing

Critical Issues in System Design

Given a performance bound we seek to:

- Min Mass of structure
 - Min Energy for control
- } MME design

– Enabling technologies for MME design:

- Minimal mass structures (tensegrity)
- Information Architecture (integrate choice of sensor/actuator networks, sensor & computational precisions, and control or estimation laws)
- Deployment schemes (origami/tensegrity)
- Model improvements from data

Information Architecture

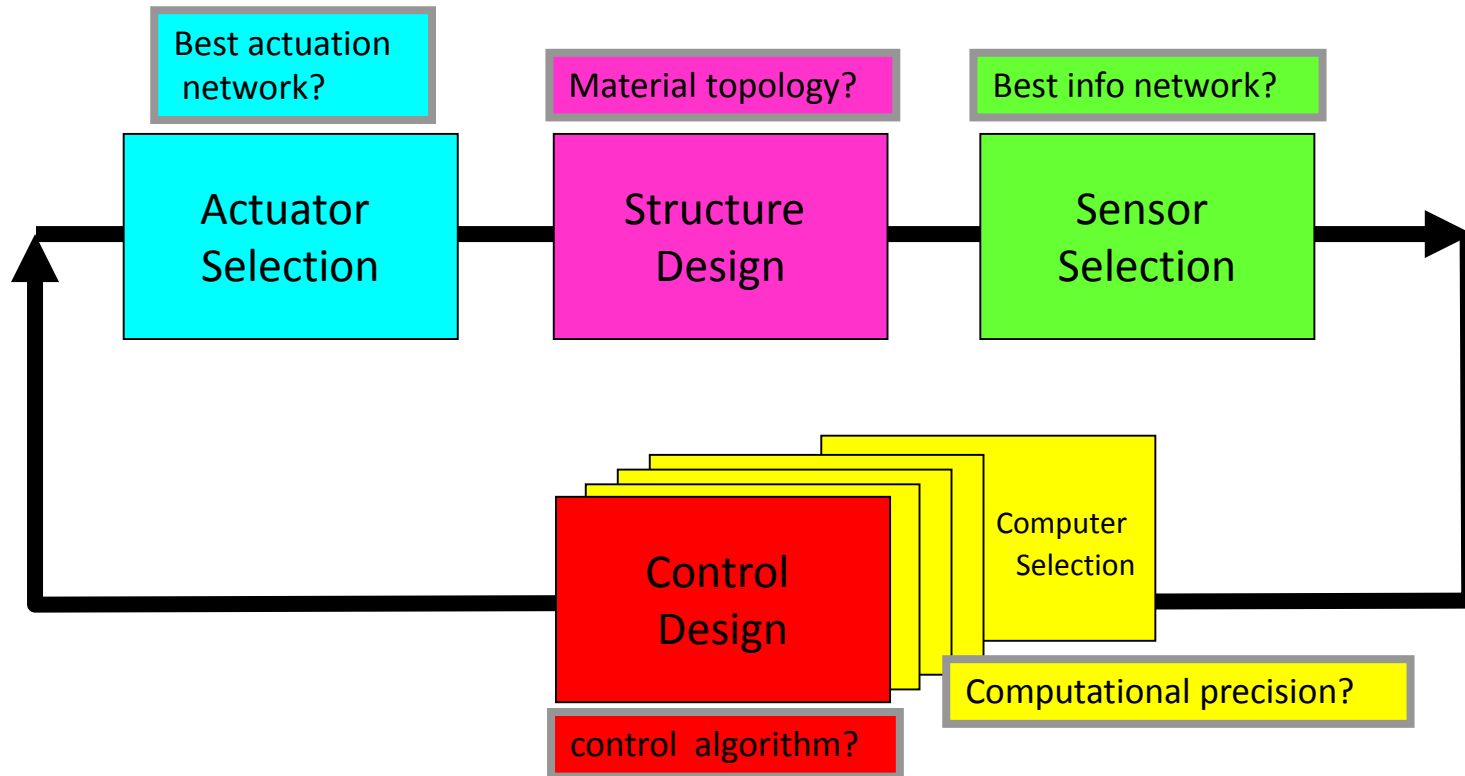
What to **measure/actuate/compute**?

With what **precision**?

With what **control law**?

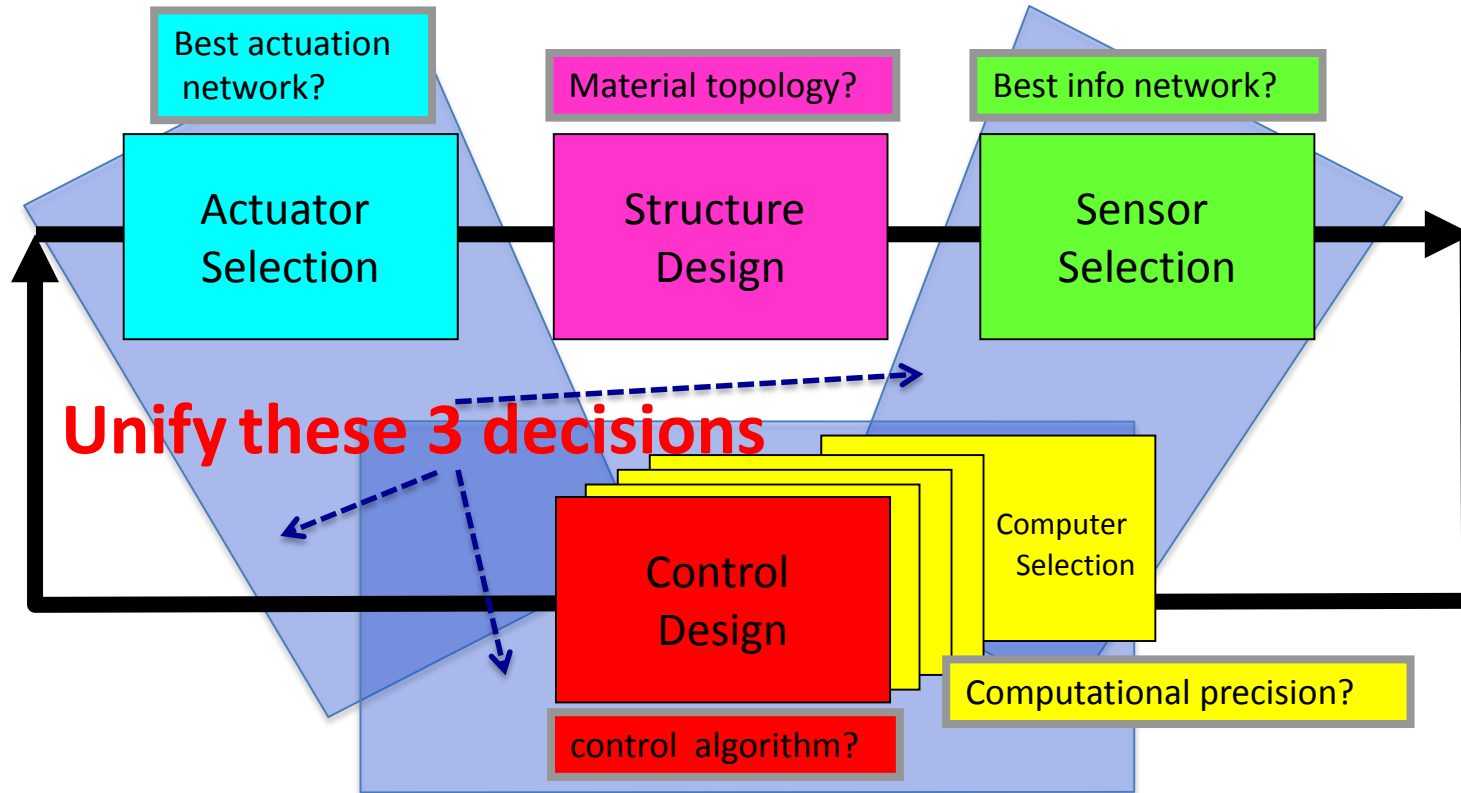
With what **cost**?

**How to integrate
these choices?**



Information Architecture

(What to **measure/actuate/compute**? With what **precision**?
With what **control law**? With what **cost**?)



Information Architecture [Skelton 2009] **jointly** optimizes:
1) control law and **2) sensor/actuator network**
(proves this is a convex problem if dynamics linear)

Conclusions

(the set of new analytical tools)

- **Control theory has been extended to:** select the precision and location required of all instruments while satisfying prespecified bounds on:
 - Total instrument costs
 - Performance errors
 - Control energy
- **Analytical tools are available to:** integrate origami and tensegrity designs of deployable structures, with shape control.
- **Analytical tools are available to:** generate all linear models which can identically match the data (a specified number of autocorrelations and cross-correlations of input/output data)

Information Architecture and Control

Plant: $\dot{x}_p = A_p x_p + B_p u + D_p w$

Output: $y = C_p x_p + B_y u$

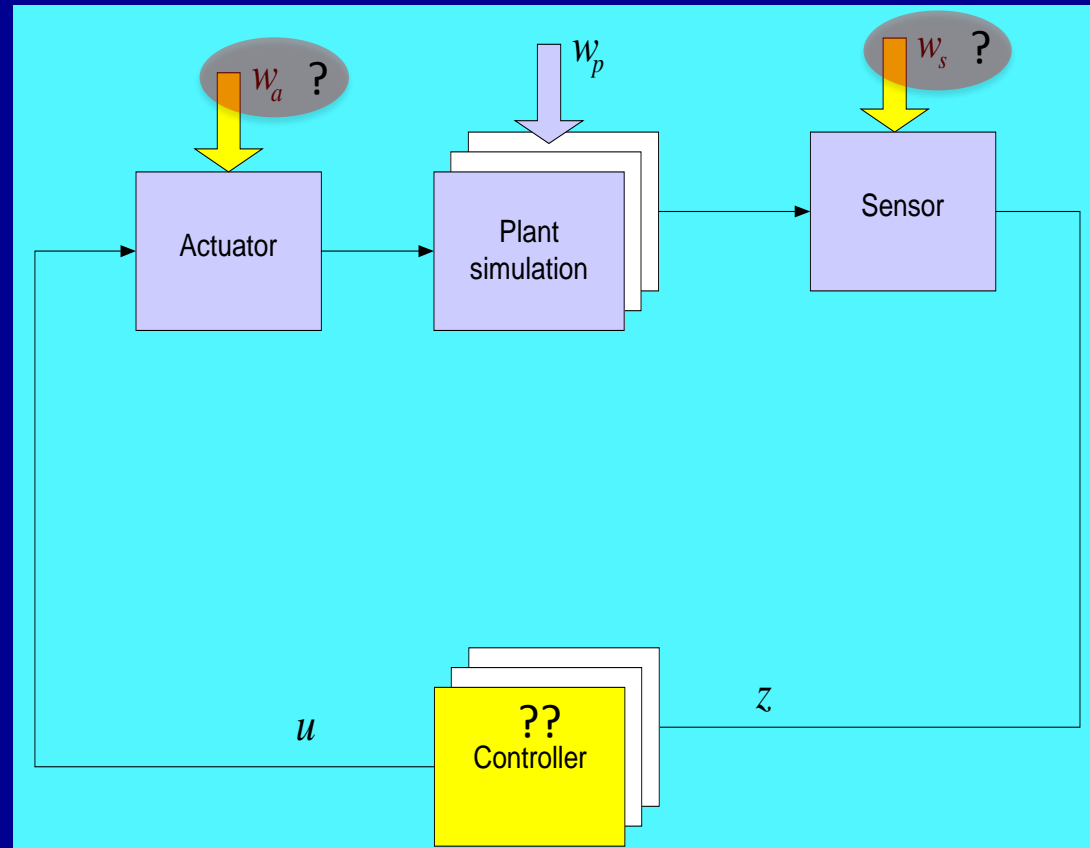
Measurement: $z = M_p x + D_z w$

$$E \begin{bmatrix} w_a \\ w_s \\ w_p \end{bmatrix} = 0, \quad E \begin{bmatrix} w_a(t) \\ w_s(t) \\ w_p(t) \end{bmatrix} \begin{bmatrix} w_a(\tau) \\ w_s(\tau) \\ w_p(\tau) \end{bmatrix}^T = \begin{bmatrix} W_a & 0 & 0 \\ 0 & W_s & 0 \\ 0 & 0 & W_p \end{bmatrix} \delta(t - \tau)$$

Controller **G**: $\dot{x}_c = A_c x_c + B_c z$
 $u = C_c x_c + D_c z$

Find **G** such that

$$\left. \begin{aligned} E[uu^T] &< \bar{U} \\ E[yy^T] &< \bar{Y} \end{aligned} \right\} \text{convex}$$



Information Architecture and Control

Plant: $\dot{x}_p = A_p x_p + B_p u + D_p w$

Output: $y = C_p x_p + B_y u$

Measurement: $z = M_p x + D_z w$

$$E \begin{bmatrix} w_a \\ w_s \\ w_p \end{bmatrix} = 0, \quad E \begin{bmatrix} w_a(t) \\ w_s(t) \\ w_p(t) \end{bmatrix} \begin{bmatrix} w_a(\tau) \\ w_s(\tau) \\ w_p(\tau) \end{bmatrix}^T = \begin{bmatrix} W_a & 0 & 0 \\ 0 & W_s & 0 \\ 0 & 0 & W_p \end{bmatrix} \delta(t-\tau)$$

$\$:= \text{tr} P W^{-1}$

$$W^{-1} := \begin{bmatrix} W_a^{-1} & 0 \\ 0 & W_s^{-1} \end{bmatrix}$$

Controller **G**:

$$\begin{aligned} \dot{x}_c &= A_c x_c + B_c z \\ u &= C_c x_c + D_c z \end{aligned}$$

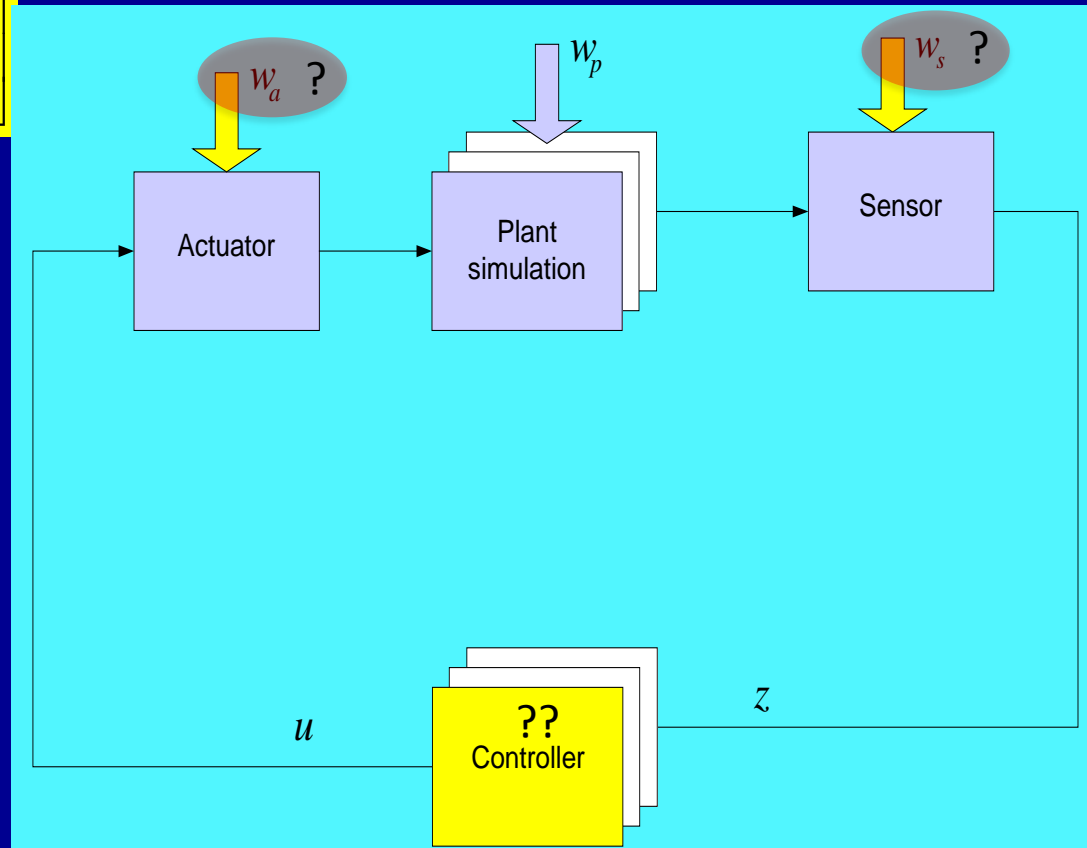
Find **W** and **G** such that

$$\$ < \bar{\$}$$

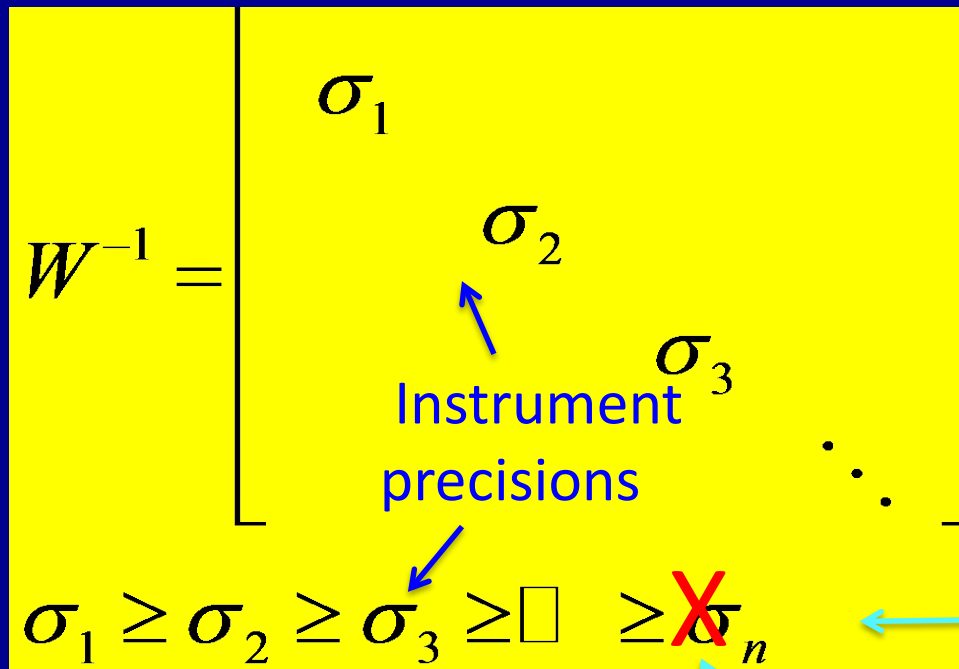
$$E[uu^T] < \bar{U}$$

$$E[yy^T] < \bar{Y}$$

Convex!



Sensor/Actuator Network Selection



$\$ \leq \bar{\$}$ Money
 $E[yy^T] \leq \bar{Y}$ Performance
 $E[uu^T] \leq \bar{U}$ Energy
Convex problem

After solving convex problem
Observe this ranking

Delete smallest precision instrument and repeat convex problem with smaller set of Instruments .
Stop when feasibility is lost